



**LARICINA**  
E N E R G Y L T D.

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**Thermal Recovery Processes in  
Clastic and Carbonate Rock**

January 31, 2013

# Contents

## Sub-Surface

- Principles of SAGD and CSS
- Pressure and Temperature
- Steam Properties
- Bitumen Phase Behavior
- Geo-Mechanics
- Relative Permeability Hysteresis
- Numerical Simulations
- SOR vs. RF or NPV vs. Cash Flow
- Carbonates

## Not Addressed:

- impact of temperature cycles on well failure
- operation of cycles with increasing duration
- higher P/T conditions in facility
- H<sub>2</sub>S, CO<sub>2</sub>

## DISCLAIMER

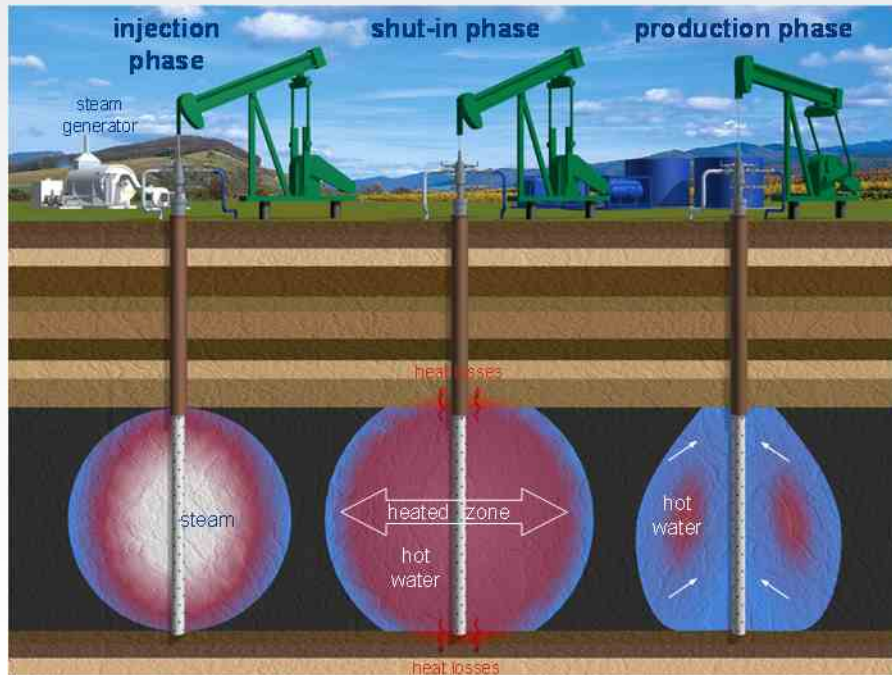
(for the experts)

- simplification
- generalization



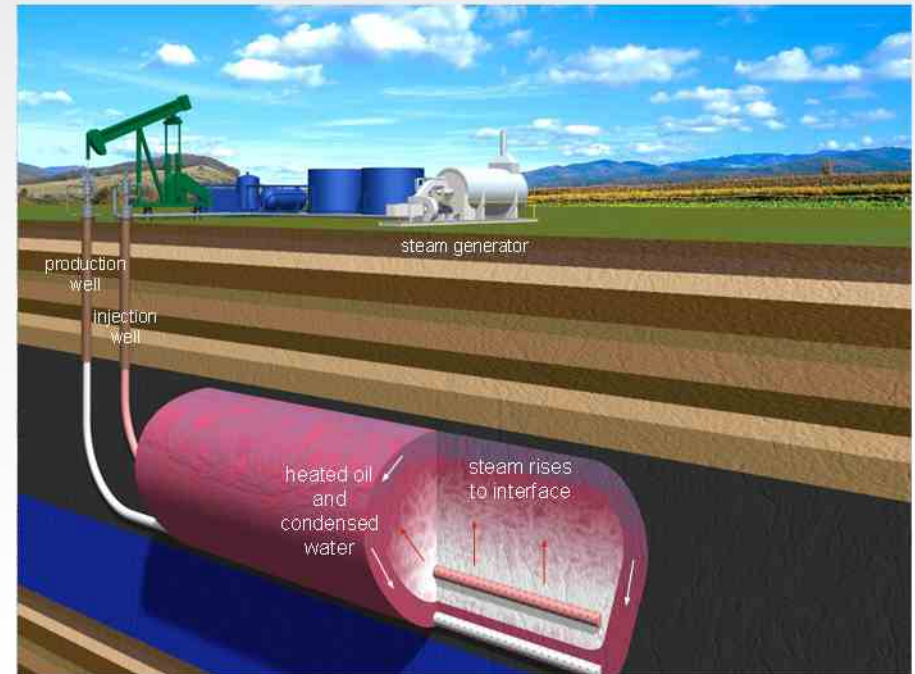
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# Principles



## CSS – Cyclic Steam Stimulation

- injection-soak-production
- vertical or horizontal wells
- dilation compaction
- solution gas drive
- gravity drainage (if mature)



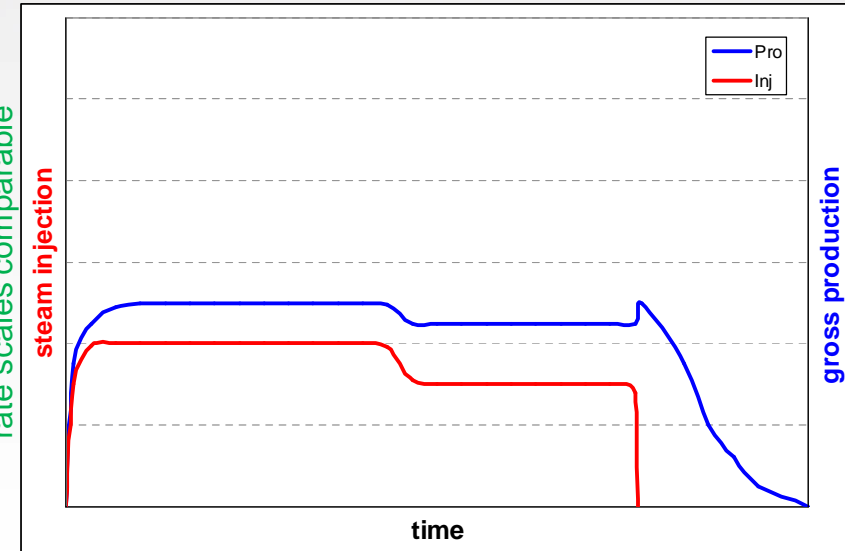
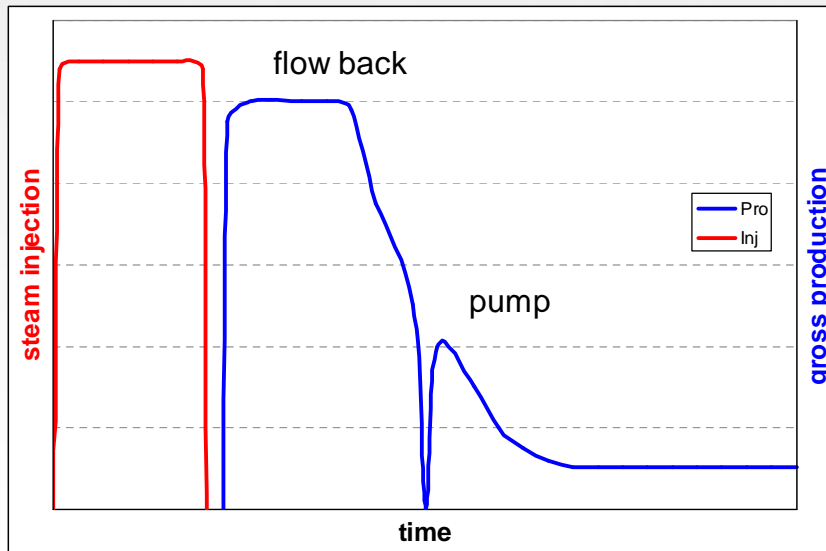
## SAGD – Steam Assisted Gravity Drainage

- balanced injection and production
- horizontal wells
- gravity drainage



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# Injection and Production



time scales not comparable

## CSS – Cyclic Steam Stimulation

- soak period after injection
- flow back initially restricted
- late production in mature CSS: gravity drainage

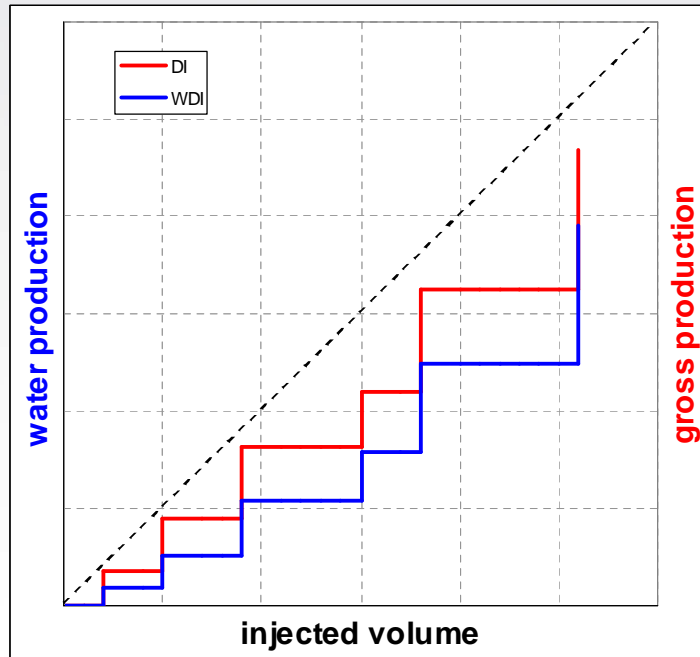
## SAGD – Steam Assisted Gravity Drainage

- balance injection and production
- produce most injected steam as water

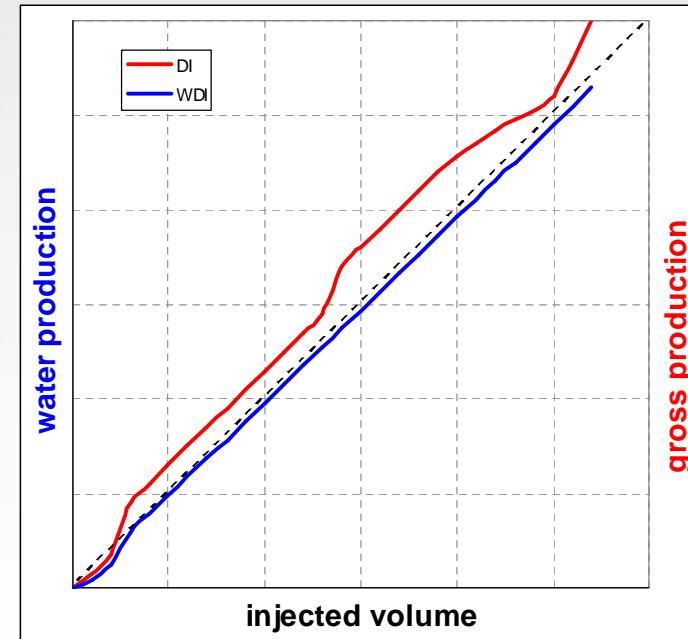


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# Material Balance



volume scales not comparable



volume scales not comparable

## CSS – Cyclic Steam Stimulation

- $1 > DI > WDI$
- liquid volume is left behind
- irreversible porosity increase
- loss to the outside

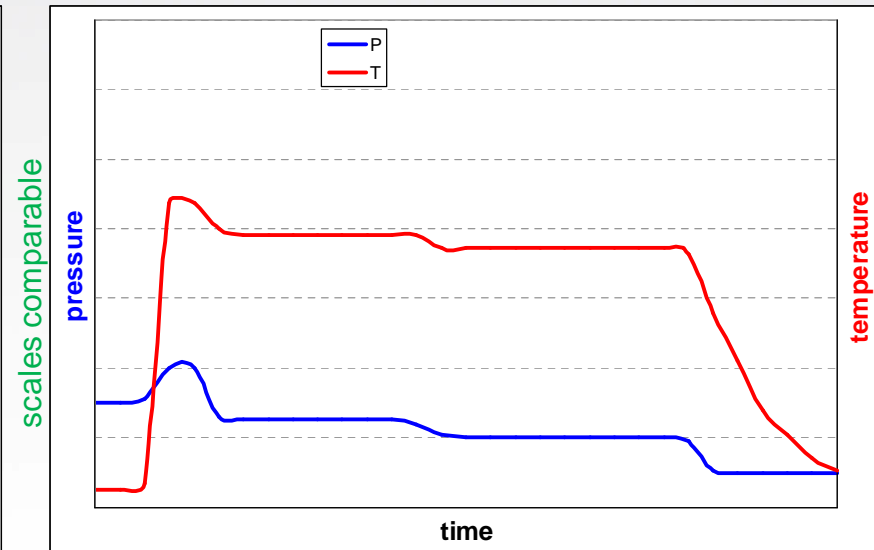
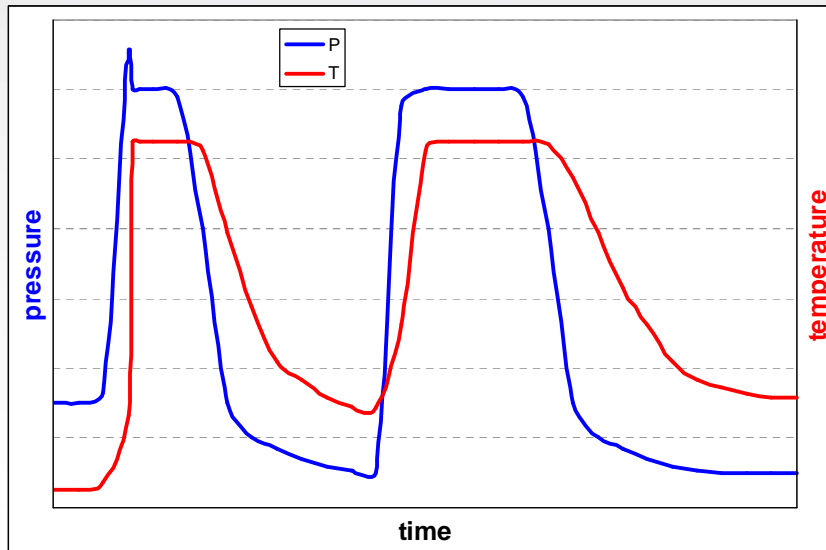
## SAGD – Steam Assisted Gravity Drainage

- $DI > 1 \approx WDI$
- liquid volume is missing
- void occupied by gas ( $H_2O$ , HC)



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# Pressure and Temperature



time scales not comparable

## CSS – Cyclic Steam Stimulation

- steam volumes increase
- initial flow back, then pump
- cycles get longer

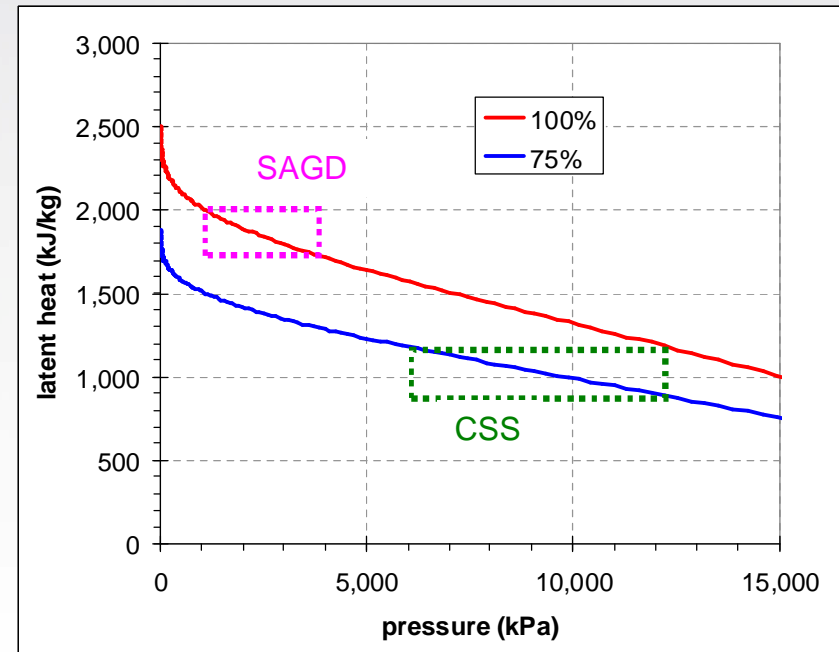
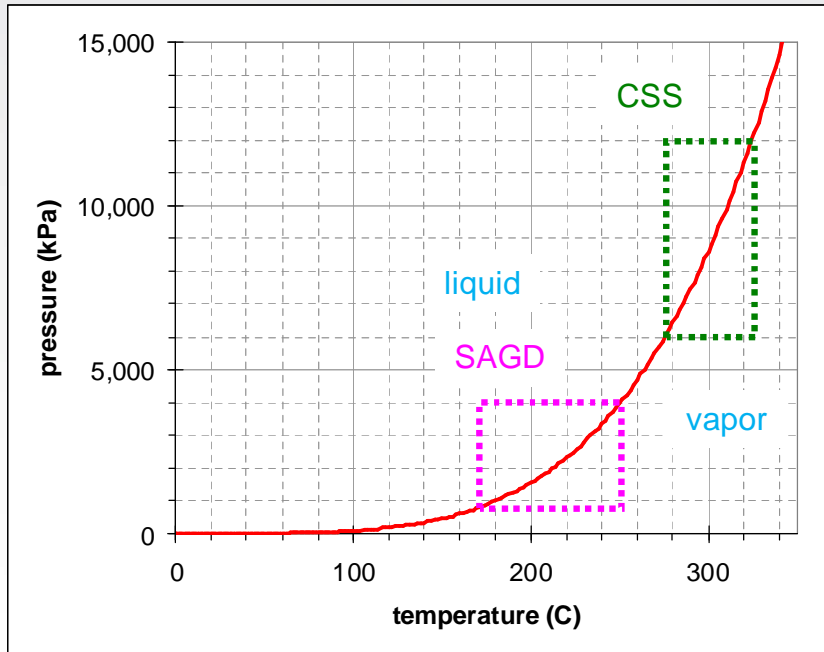
## SAGD – Steam Assisted Gravity Drainage

- operating pressure determines the temperature
- blow-down in late life



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# Steam Properties



## CSS – Cyclic Steam Stimulation

- higher steam P&T
- lower quality (variable  $P_{inj}$ )
- reduce viscosity
- main drive mechanism: dilation/re-compaction
- create volume

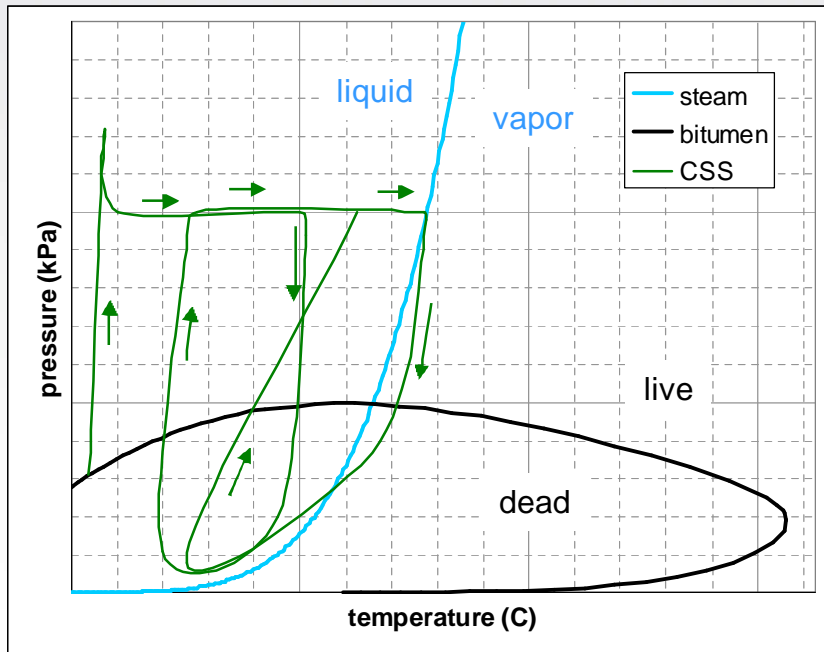
## SAGD – Steam Assisted Gravity Drainage

- moderate steam P&T
- less volume required for latent heat
- reduce viscosity
- main drive mechanism: gravity drainage
- maintain gas phase in chamber



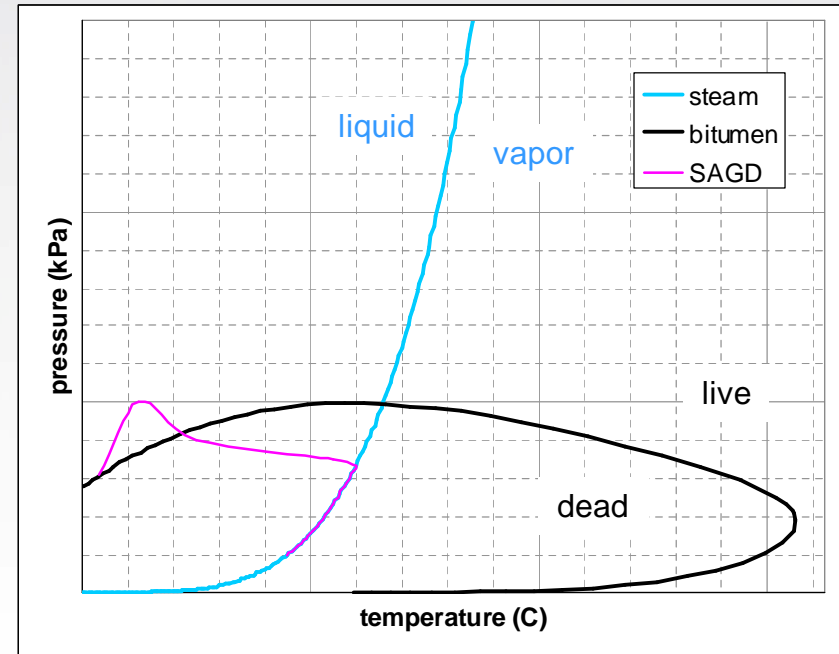
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# Phase Behavior



## CSS – Cyclic Steam Stimulation

- high P keeps bitumen live during 1<sup>st</sup> cycle injection
- if gas is abundant, bitumen can re-saturate



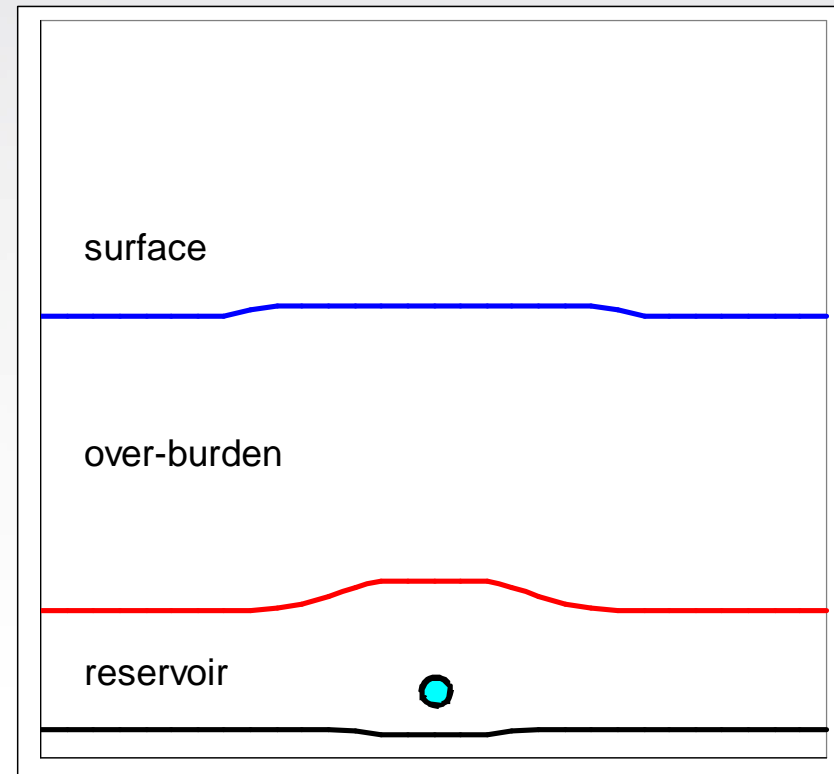
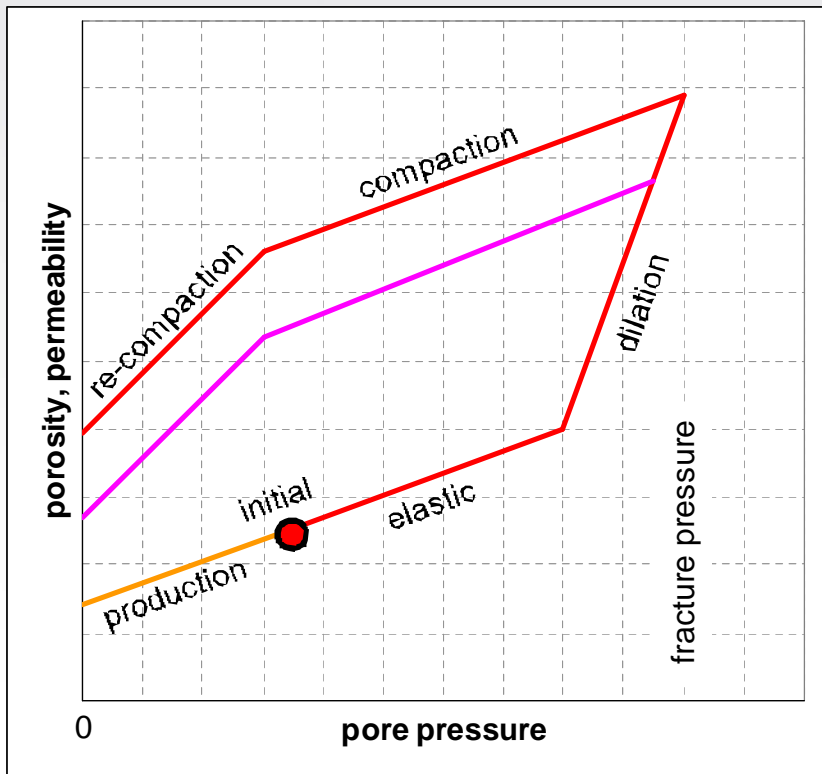
## SAGD – Steam Assisted Gravity Drainage

- temperature leads to dead bitumen fast
- no potential re-saturation





# Deformation



## CSS – Cyclic Steam Stimulation

- full range of pressure cycle
- compaction is main drive mechanism
- irreversible dilation  $\Rightarrow$   $DI < 1$

## SAGD – Steam Assisted Gravity Drainage

- low range of pressure
- thermal expansion



# Fracturing

overburden weight

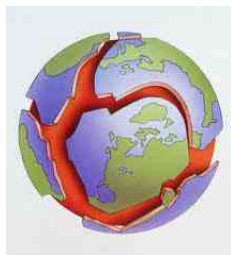
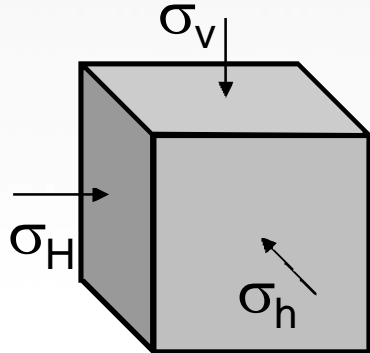
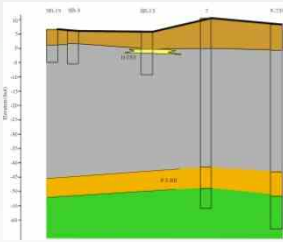
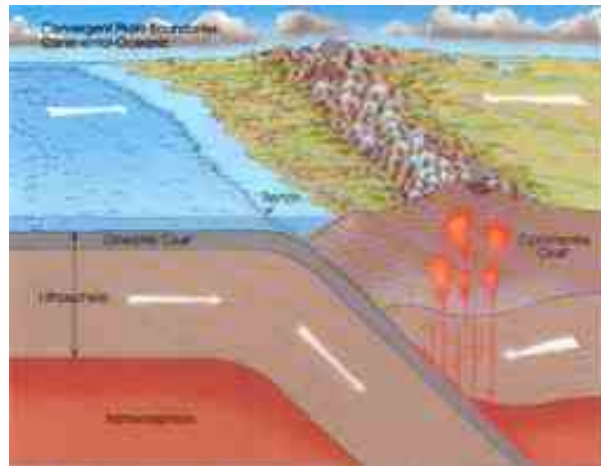
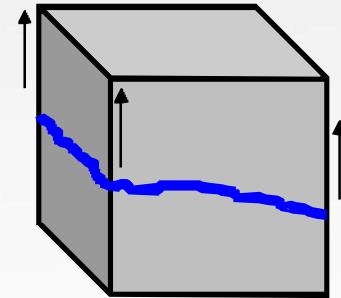


plate tectonics

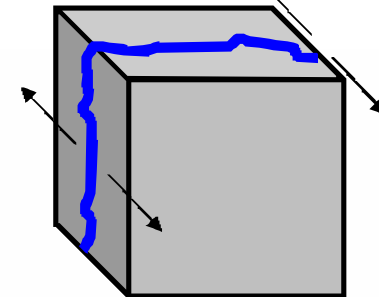
once the pore pressure exceeds the smallest stress, and the rock strength is overcome, the rock will break



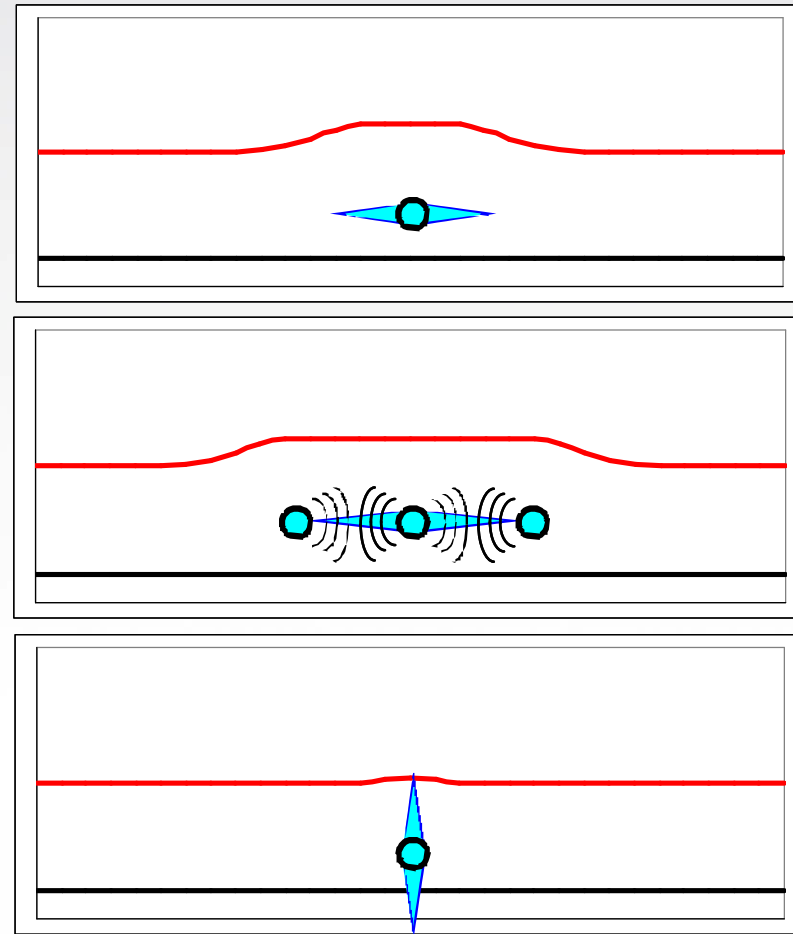
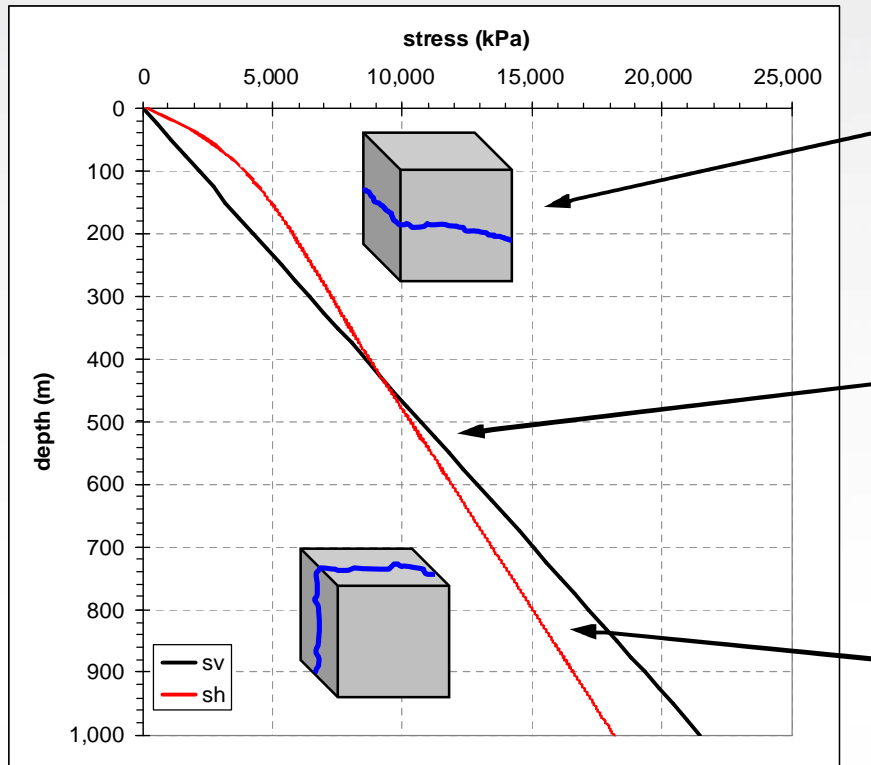
$$\sigma_v < \sigma_h$$



$$\sigma_h < \sigma_v$$

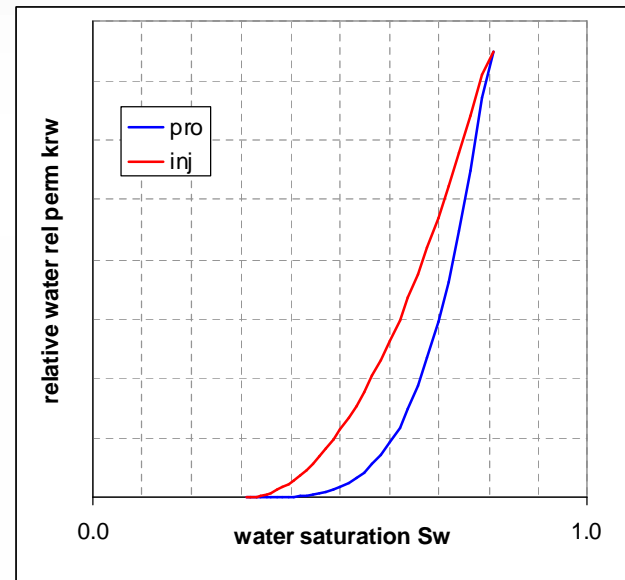
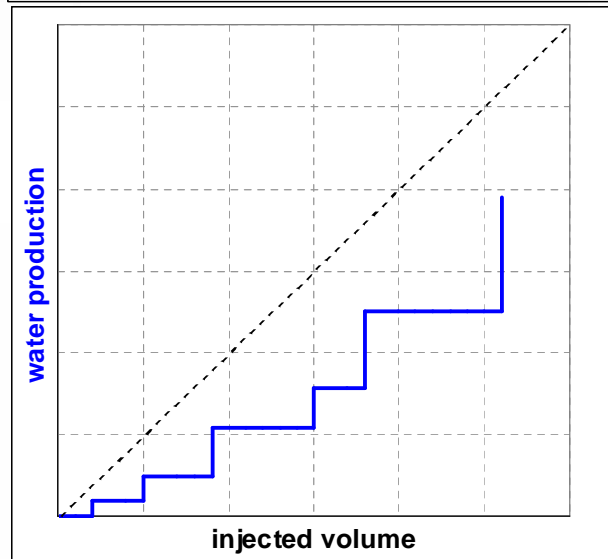
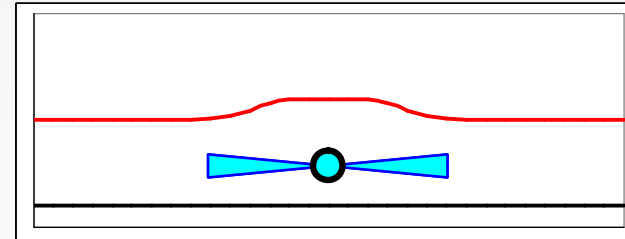
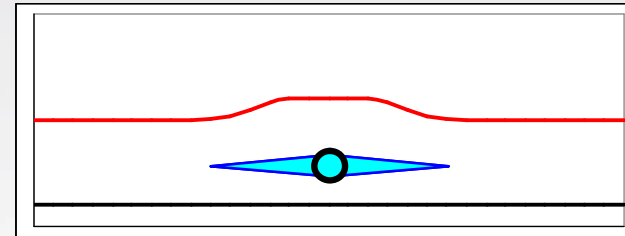


# Fracturing cont'd



thermo- and poro-elastic effects of multiple wells can turn fracture orientation from initially vertical to horizontal

# Relative Permeability Hysteresis



# Numerical Simulations

## CSS

- inj/pro cycles, unstable
- large range of P&T
- sand-face steam quality
- bitumen phase behavior
- large cycles of  $S_w$  and  $S_o$
- critical gas saturation
- rel perm hysteresis
- dilation hysteresis
- fracture initiation, growth
- fracture flow

## SAGD

- balanced inj/pro
- small range of P&T
- no issue
- mainly dead bitumen
- stable  $S_w$  and  $S_o$  changes
- initial gas saturation
- not necessary
- not necessary
- not necessary
- not necessary



# Performance Comparison

## **CSS** (CNRL)

Pads 29-31

Primrose South

- Clearwater
- 12 m net pay
- 3 pads, each  
2 x 8 hor wells
- spacing 190 m
- length 1,200 m
- since 2004

## **SAGD** (Suncor, CNRL)

Burnt Lake Pilot

Primrose East

- Clearwater
- 25 m net pay
- 3 SAGD well pairs
- spacing 80 m
- length 700; 900, 1000 m
- since 1997



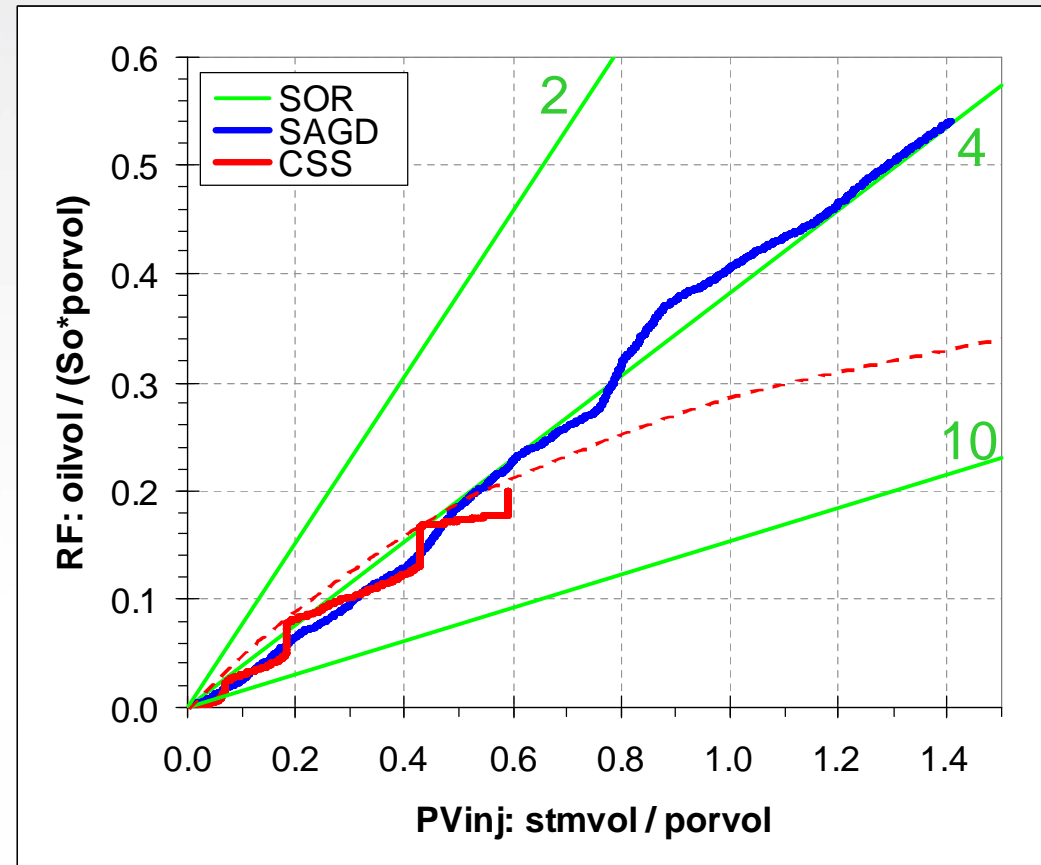
# Recovery Factor

## CSS:

- RF is not a fixed number
- cut-off SOR is economic decision

## SAGD:

- stable thermal efficiency
- RF > 60 possible at stable SOR

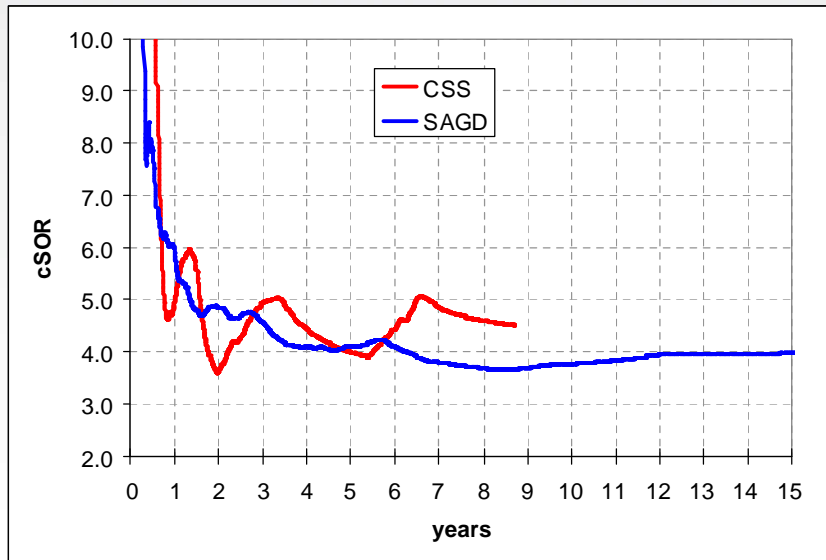


no time relation



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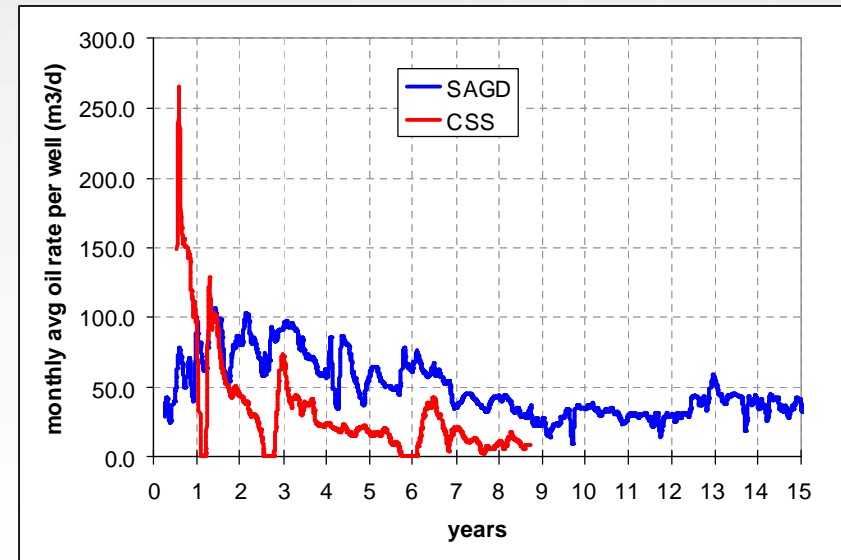
# Time Dependent



full pad performance

CSS:

- lower SOR after Cy1 and Cy2
- equivalent SOR after Cy3
- higher SOR after Cy4+



individual well performance

CSS:

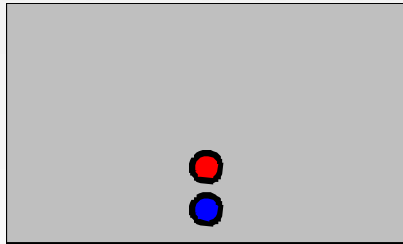
- 3-6 x rates in Cy1
- equivalent rates in Cy2
- much lower rates in Cy3+



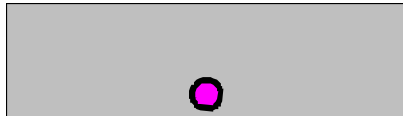
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# Economic Difference



- 2x net pay
- 2x wells
- higher SOR after 2 yrs
- lower oil rates in 1<sup>st</sup> yr
- SOR stable for 10+ yrs
- RF > 60% achievable in 10+ yrs



- ½ net pay
- ½ wells
- lower SOR after 2 yrs
- 3-6 x oil rates in 1<sup>st</sup> yr
- cut-off SOR at 20% RF

CSS: lower capital and fast return –

**NPV**

SAGD: sustainable SOR and high RF for additional 5-10 yrs – **cash flow**



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# Consider this ...

- start dev't with CSS to maximize NPV
- transform mature CSS to SAGD to maximize RF
- attempts by IOL, CNRL, SCAN
- risk of CSS in shallow reservoirs is over-rated
  - stress regime favors horizontal fractures
  - initial SAGD injection pressures are comparable to CSS requirements for dilation
  - CSS vs. SAGD operation strategy in case of increased injectivity
- SAGD has advantage of control over operation pressure
  - now high or low pressures required
  - gas cap
  - top/bottom water
- permeability may be too high for CSS
  - high pressures not achievable
  - example: fractured carbonates

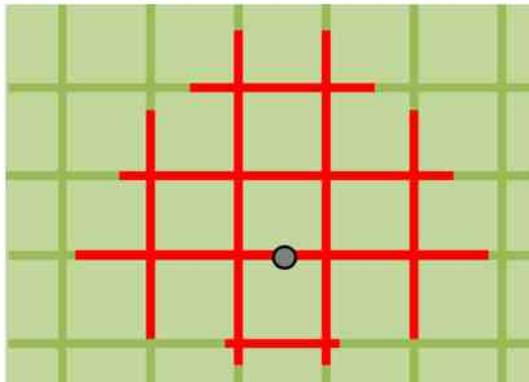
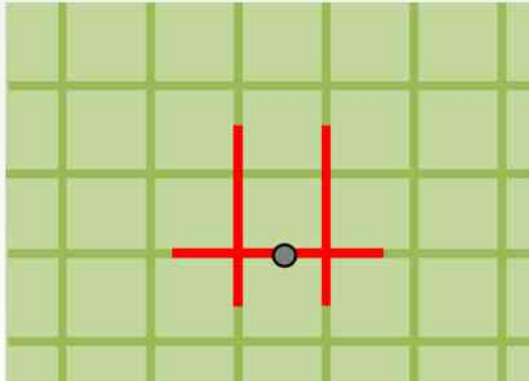


# What to do in Carbonates?

- fractures in carbonates increase effective permeability
- high permeability is good for SAGD but for CSS, this may prevent reaching injection pressures that cause dilation - the second 'S' in CSS
- very high permeability may cause uncontrollable shortcut between injector and producer of classic SAGD pair
- distributions of primary and secondary porosity vary within the Grosmont, and the recovery process has to be adapted
- conceptual process for carbonates in two phases



# Phase 1: Cyclic SAGD



## Cyclic

### objectives:

- heat fracture system by convection
- recover bitumen in fractures

### recovery mechanisms:

- fractures
  - gravity
  - thermal expansion
- matrix
  - thermal expansion
  - solution gas drive

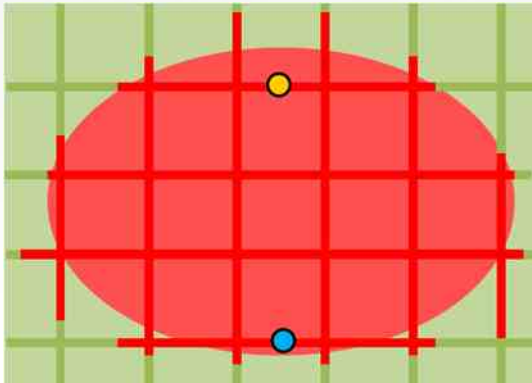


decreasing contribution  
to total bitumen production



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# Phase 2: Continuous SAGD



requires dedicated  
injector and producer

multiple options for  
configurations

## Continuous

objectives:

- maintain heat in fractures
- heat matrix by conduction

recovery mechanisms:

- matrix
  - imbibition
  - gravity
- fractures
  - serve as collectors

■ similar contribution  
to total bitumen production



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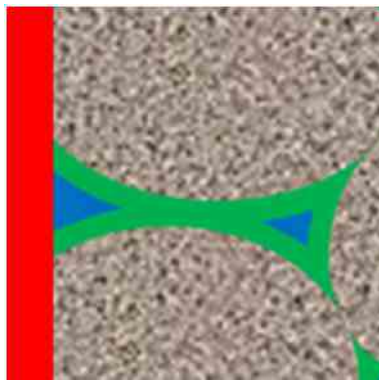
# Matrix Contributions

## Spontaneous Imbibition

### Initial (10-20 °C)

#### oil wet:

- bitumen is continuous phase
- cold bitumen is immobile
- water is immobile (non-continuous)
- hot water (condensed steam) will not enter matrix
- bitumen only move into fracture by thermal expansion
- heat will penetrate into matrix by conduction



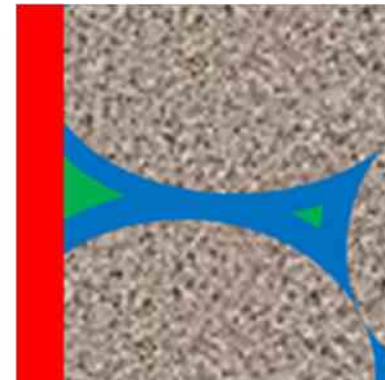
green - bitumen  
blue - water  
red - steam

### Hot (> 150 °C)

#### changes to water wet:

- water is continuous phase
- water is mobile (continuous)
- hot bitumen is mobile
- hot water (condensed steam) will be sucked into matrix
- bitumen will be pushed out of matrix into fracture
- heat will penetrate into matrix by conduction and convection
- confirmed in lab tests
- reported for Qarn Alam, Oman

SPE 71866, SPE 153812



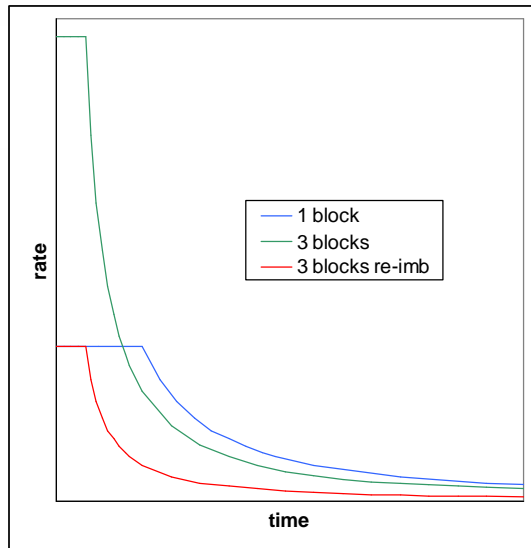
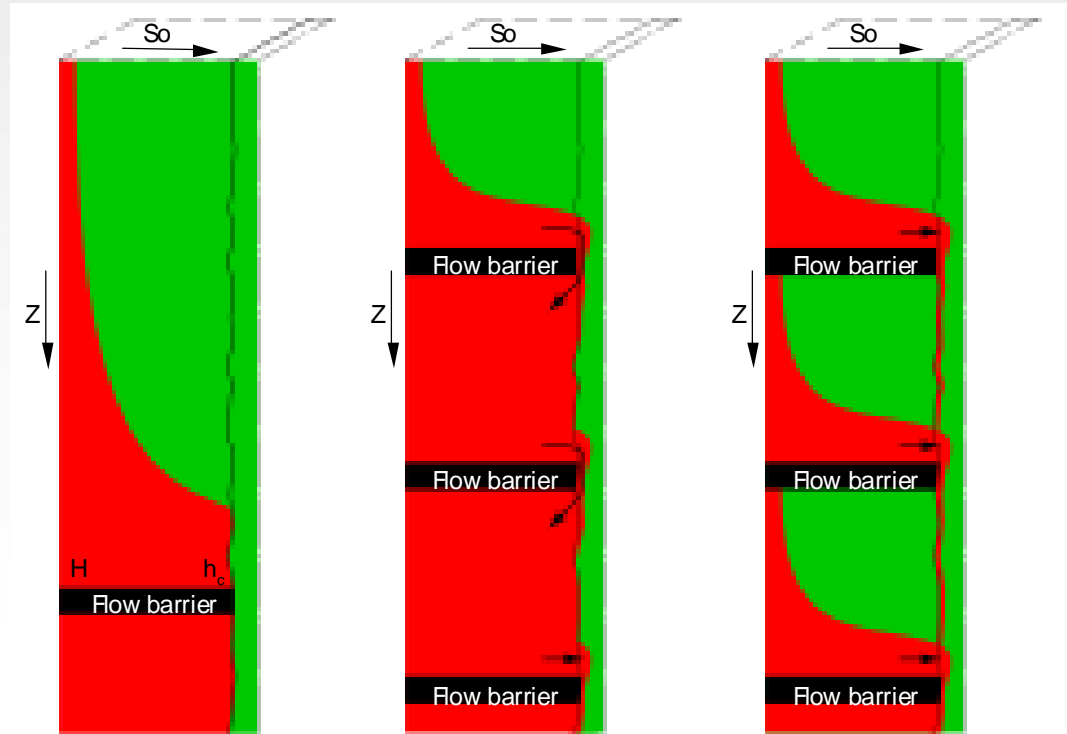
# Matrix Contributions Gravity Drainage

**gravity drainage rate depends on:**

- density contrast steam/bitumen
- vertical permeability
- oil viscosity

**example:**

- 1,000 m well length
- 100 m well spacing
- 100 mD matrix vertical permeability
- 100 cP viscosity
- 700 m<sup>3</sup>/d drainage rate (theoretical)



red- bitumen  
 blue - water  
 green - gas or steam

SPE 111403



# Summary

- Conventional SAGD in Clastic Reservoirs
  - relies on gravity
  - usually associated with a well pair at the bottom and 5-8 m vertical distance
  - oil rates and SORs are stable over a long time, allowing high RF
- Conventional CSS in Clastic Reservoirs
  - relies initially on dilation and re-compaction; later on gravity
  - usually associated with single well operated at high pressures
  - oil rates peak in first 1-3 cycles; then performance is below SAGD
- Cyclic SAGD in Carbonates
  - dilation unlikely; no CSS benefits; relies on gravity
  - targets bitumen in fractures
- Continuous SAGD in Carbonates
  - gravity drainage and spontaneous imbibition
  - targets bitumen in matrix

